

<sup>3</sup> Rodden, W. P. and Revell, J. D., "The Status of Unsteady Aerodynamic Influence Coefficients," Paper FF-33, presented to IAS 30th Annual Meeting, Jan. 22-24, 1962; preprinted as Rept. TDR-930(2230-09)TN-2, Nov. 22, 1961, Aerospace Corp., El Segundo, Calif.

<sup>4</sup> Rodden, W. P., "Aerodynamic Influence Coefficients From Strip Theory," *Journal of the Aerospace Sciences*, Vol. 26, No. 12, Dec. 1959, pp. 833-834.

<sup>5</sup> Hassig, H. J., "An Approximate True Damping Solution of the Flutter Equation by Determinant Iteration," *Journal of Aircraft*, Vol. 8, No. 11, Nov. 1971, pp. 885-889.

<sup>6</sup> Members of the Aerodynamics and Structures Research Organization of The Boeing Company, "An Analysis of Method for Predicting the Stability Characteristics of an Elastic Airplane; Appendix B: Methods for Determining Stability Derivatives," CR-73275, Nov. 1968, NASA.

<sup>7</sup> Bergh, H. and Zwaan, R. J., "A Method for Estimating Unsteady Pressure Distributions for Arbitrary Vibration Modes from Measured Distributions for One Single Mode," Rept. NLR-TR-F.250, Feb. 1966, National Aerospace Lab., Amsterdam, The Netherlands.

## Reply by Author to W. P. Rodden

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**T**HE comment by Rodden is a grossly unrealistic reading of Ref. 1. The following two paragraphs are quoted from this reference.

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"Comparing with thin-airfoil theory, the lift-curve slope is given exactly for any  $N$  by twice the averaged value of  $\gamma_n/V\alpha$ . Thus, for  $N=3$ ,  $c_{1\alpha} = \frac{2}{3}[(15\pi/8) + (3\pi/4) + (3\pi/8)] = 2\pi$ . Likewise the moment is given exactly for any  $N$ . Besides for the chordwise cotangent loading, the lift and moment are summed exactly for the first and second sine harmonics of chordwise loading.

The discrete chordwise loading terms  $\gamma_n/V$  are constant over a given incremental chord distance  $c/N$ . For plotting the chordwise loading,  $\gamma_n/V$  is positioned at the quarter-chord of the  $n$ th segment, that is at  $\xi_n = (n - \frac{1}{2})/N$ . A chordwise loading factor can be formed that relates  $\gamma/V$  at  $\xi_n$  with  $\gamma_n/V$ . This factor defined by  $f_n$  is the ratio of thin-airfoil theory value, Eq. (14), to the incremental loading theory value, Eq. (9)."

Much of the objective of Ref. 1 is to provide a simple, short, rigorous analysis to prove that the chordwise loading is integrated exactly for any  $N$ -paneled lattice. The first quoted paragraph shows that this  $2N$  line theory integrates exactly as the simpler 2 line theory ( $\frac{1}{2} - \frac{1}{2}$  - chord wing theory), which applies for all aspect ratios.

The second quoted paragraph concerns the problem when attempts are made to plot the chordwise loading. Although the sum of the panel elemental vortex lifts ( $2\gamma_n c/N$ ) sum up to the exact total chord lift, the chord loading  $\gamma_n$  is not necessarily the exact  $\gamma$  at chord station  $\xi_n$ . In the second quoted paragraph a loading factor,  $f_n$ , is defined which aids in plotting the chordwise loading distribution. As repeated several times in Ref. 1, for plotting, the chordwise loading at  $\xi_n$  is defined by using the chordwise loading factor as in  $\gamma/V = f_n \gamma_n/V$ . Qualitatively, this  $f_n$  factor is independent of aspect ratio. Slender wing theory shows that the leading edge loading stays as high as that resulting from two-dimensional planar thin wing theory.

I do not throw babies out with the bath water, they are too precious.

## Reference

<sup>1</sup> De Young, J., "Convergence Proof of Discrete-Panel Wing Loading Theories," *Journal of Aircraft*, Vol. 8, No. 10, Oct. 1971, pp. 837-839.